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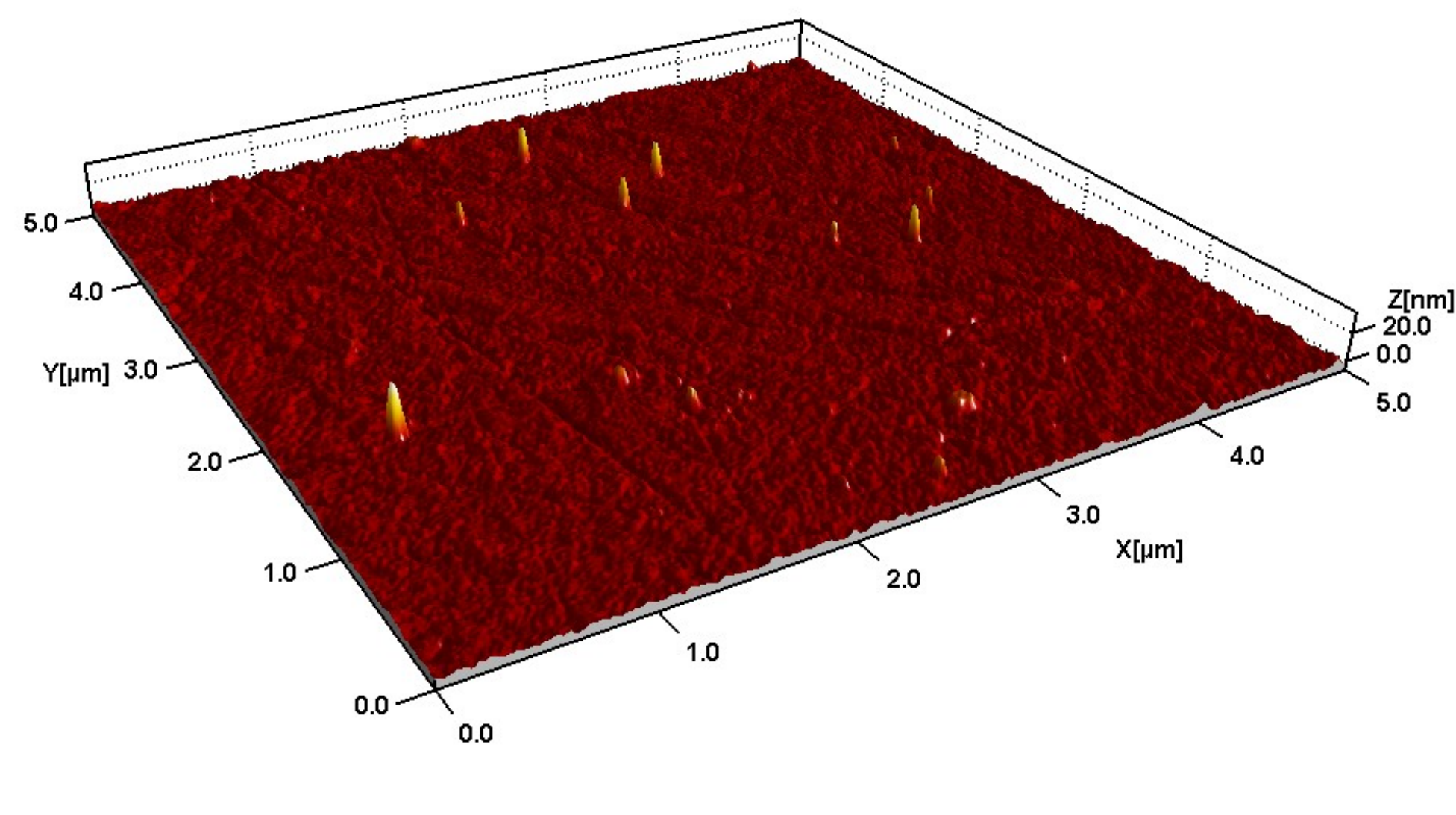
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Introduction & Experimental

Deformable sandwich sheet materials produced as raw materials and formed afterwards to complex geometries require a good bonding to guarantee a stable shear transfer between the single layers. However, due to the deformation, failures by delamination often occur between the epoxy and the metal. The aim of our work is to understand the basic effect of the interfaces' bonding behavior in selected preparation steps of the system. These effects have been investigated by means of Atomic Force Microscopy (AFM), operating in ambient air and X-ray Photoelectron Spectroscopy (XPS), operating under ultrahigh vacuum conditions.

Preparation: **1st step:** The pure steel surface was manually cleaned with acetone and isopropanol, as well as sputtered with Ar⁺ ions.
2nd step: The sample from step one was extracted from vacuum and exposed to ambient air for 2 min.
3rd step: The sample from step two is covered with an epoxy film by spin coating.

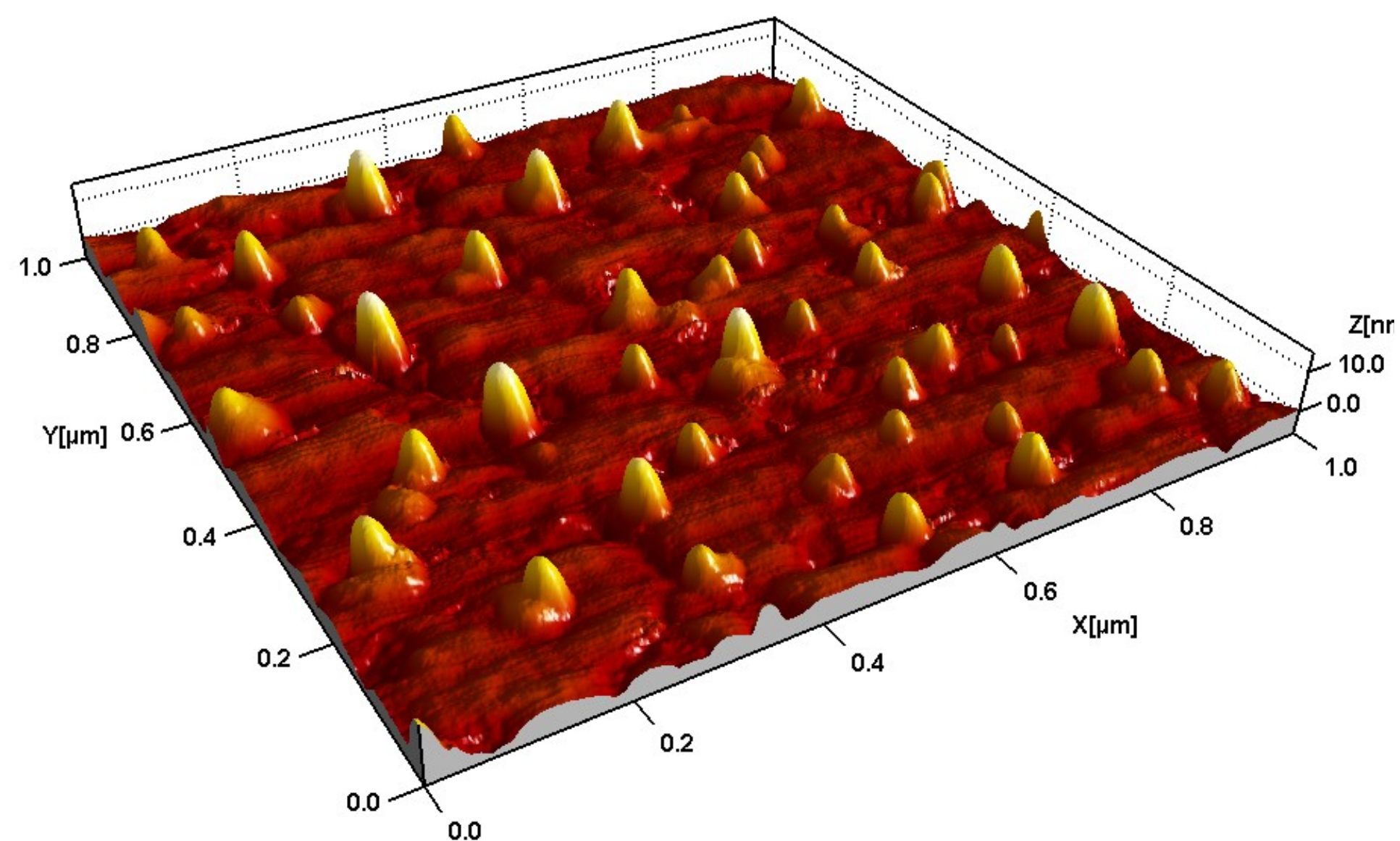
AFM 1st step



smooth surface
distinct structures
(probably aerosols)

RMS roughness: 1.5 nm
avg. diameter: 50-150 nm
mean height: 30 nm

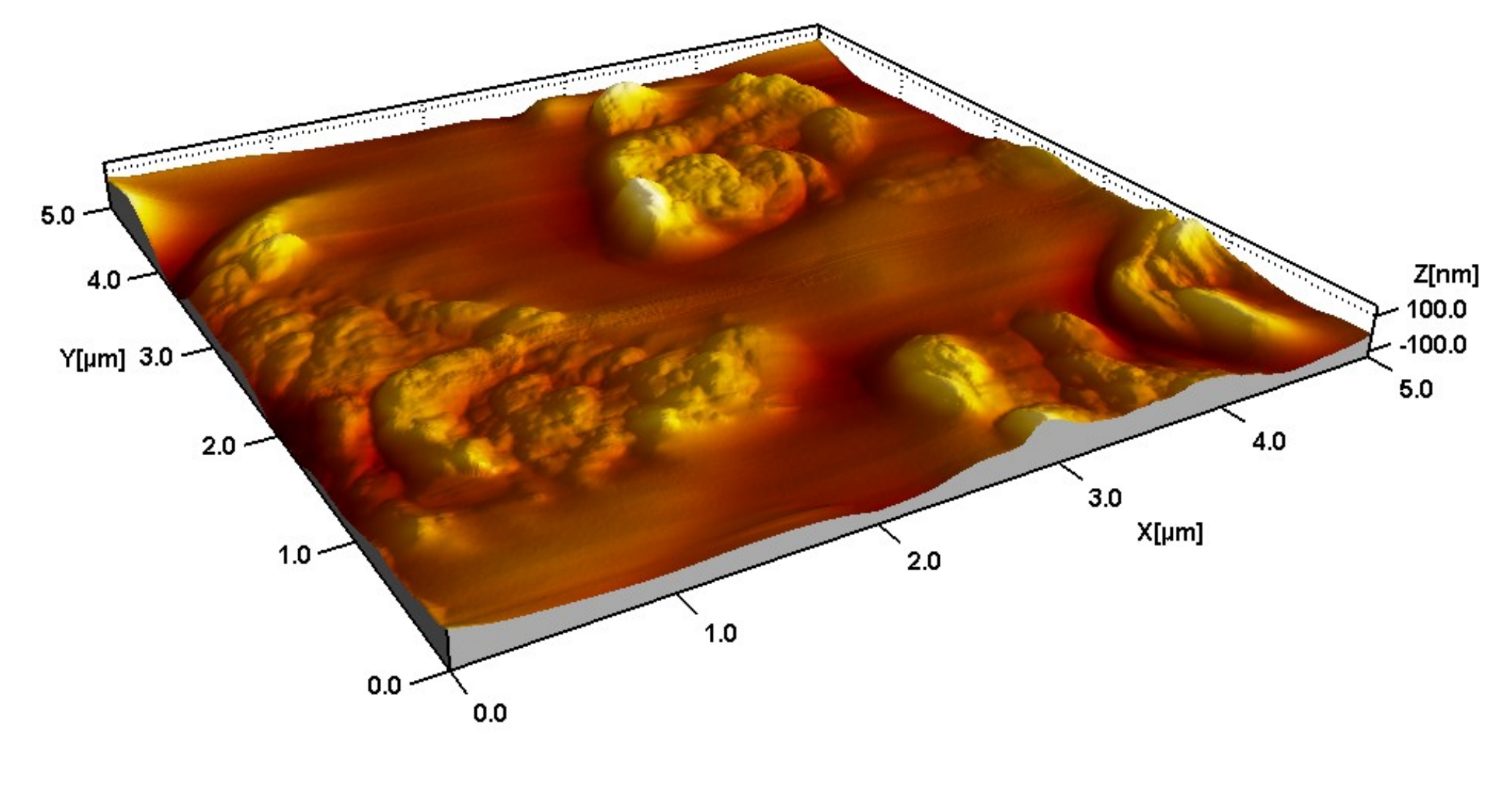
AFM 2nd step



aerosol particles
(arising from agglomeration)
within the atmosphere)

3.7 nm
129 nm
28 nm

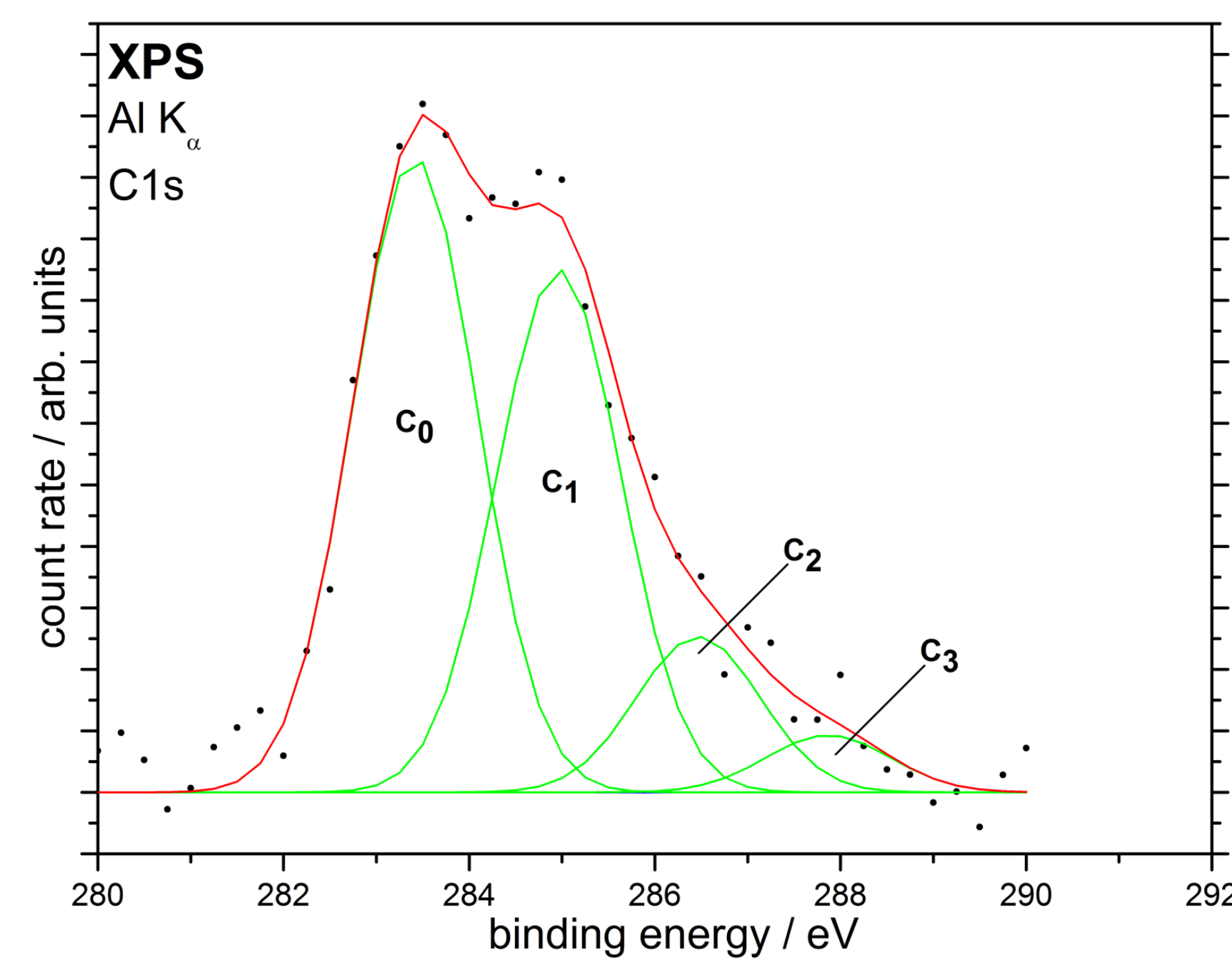
AFM 3rd step



two different domains
regions with a comparatively smooth surface
regions which exhibit noticeable aggregation of epoxy

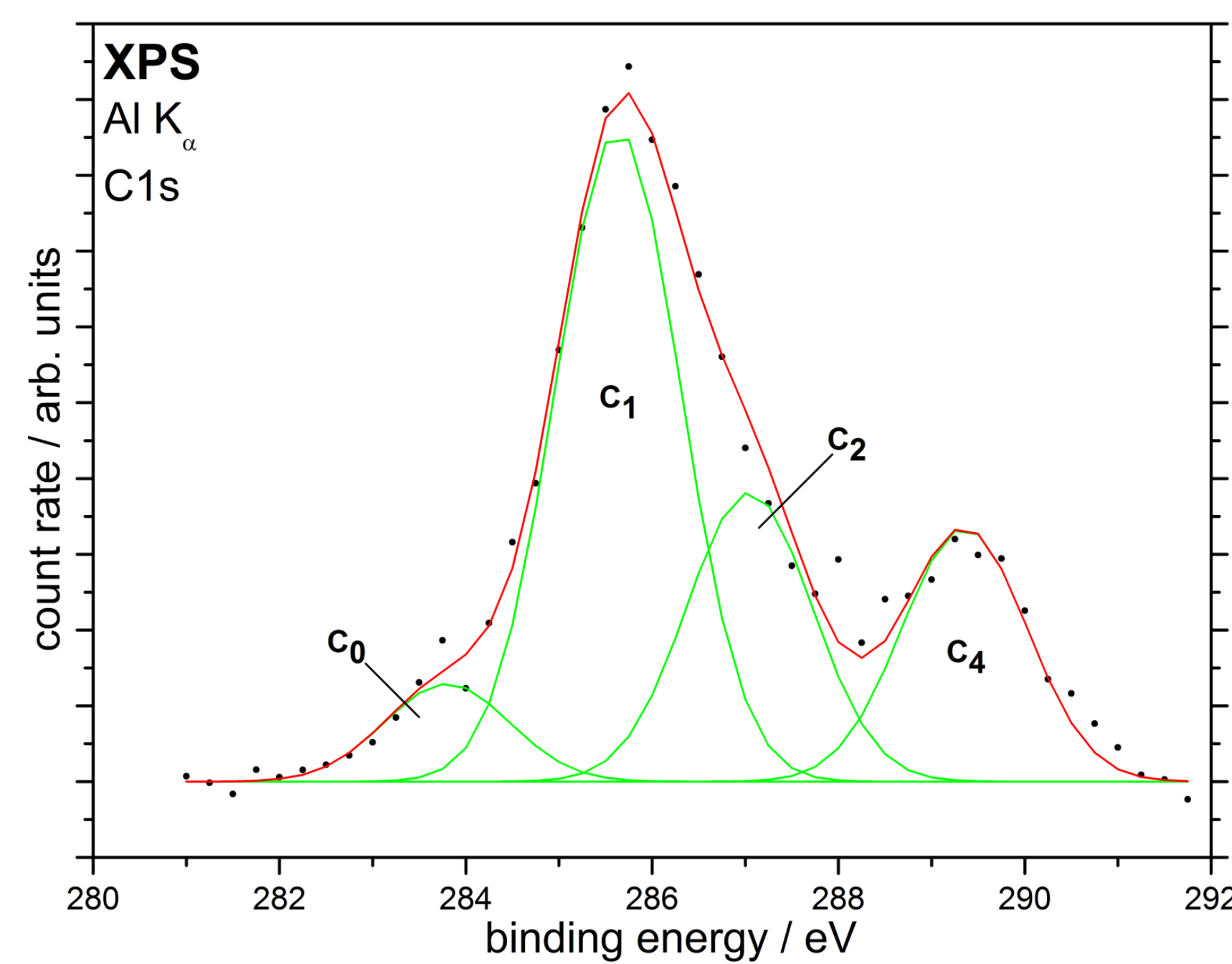
34 nm
-
-

XPS 1st step



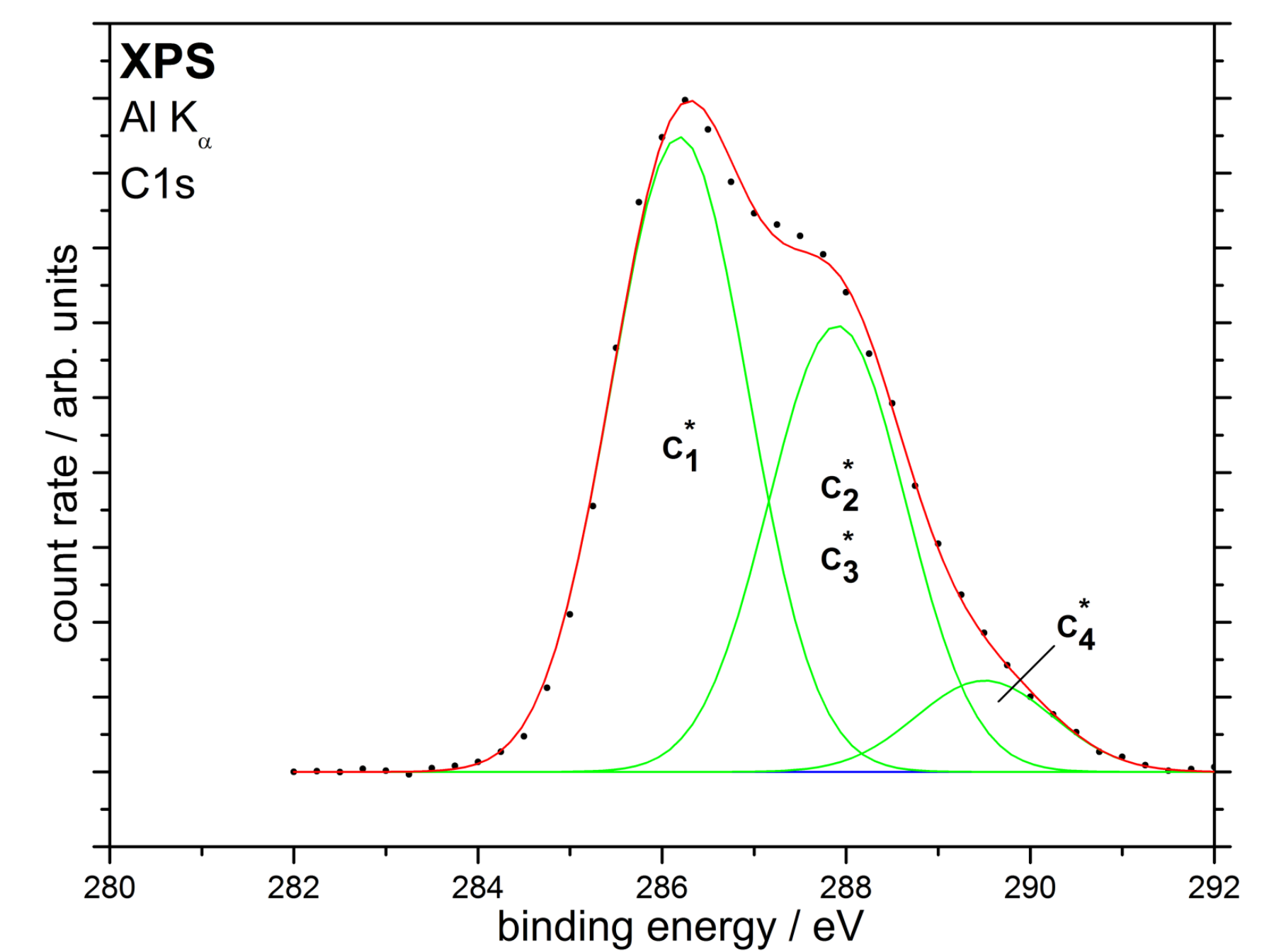
| Orbital | Peak | rel. int. | Assignment |
|---------|----------------|-----------|------------------|
| C1s | C ₀ | 46.3 % | carbide |
| | C ₁ | 38.1 % | C-C / C-H |
| | C ₂ | 11.4 % | C-O |
| | C ₃ | 4.2 % | C=O |
| Fe2p | I | 72.8 % | Fe ⁰ |
| | II | 27.2 % | Fe ²⁺ |
| | III | - | - |

XPS 2nd step

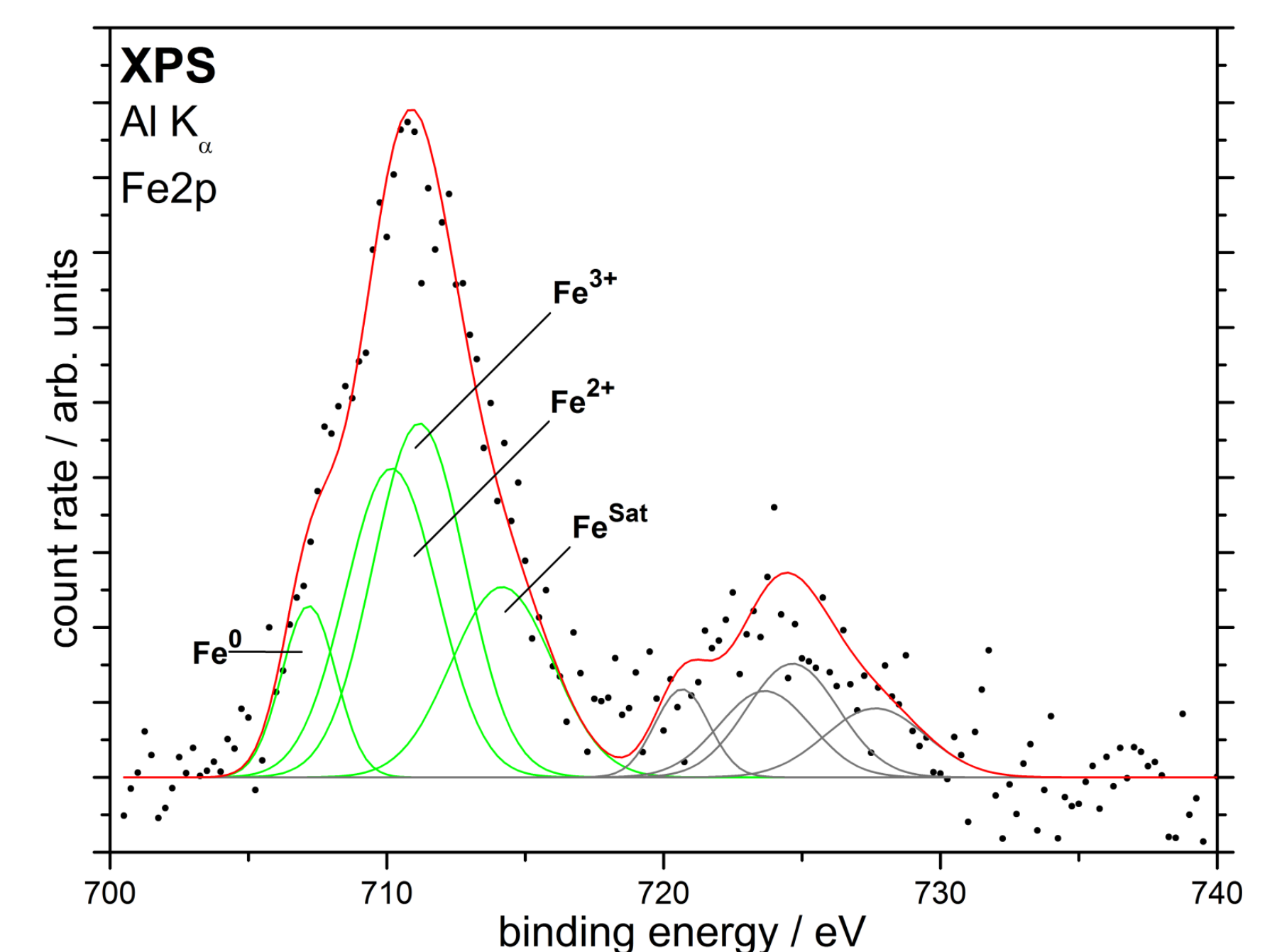
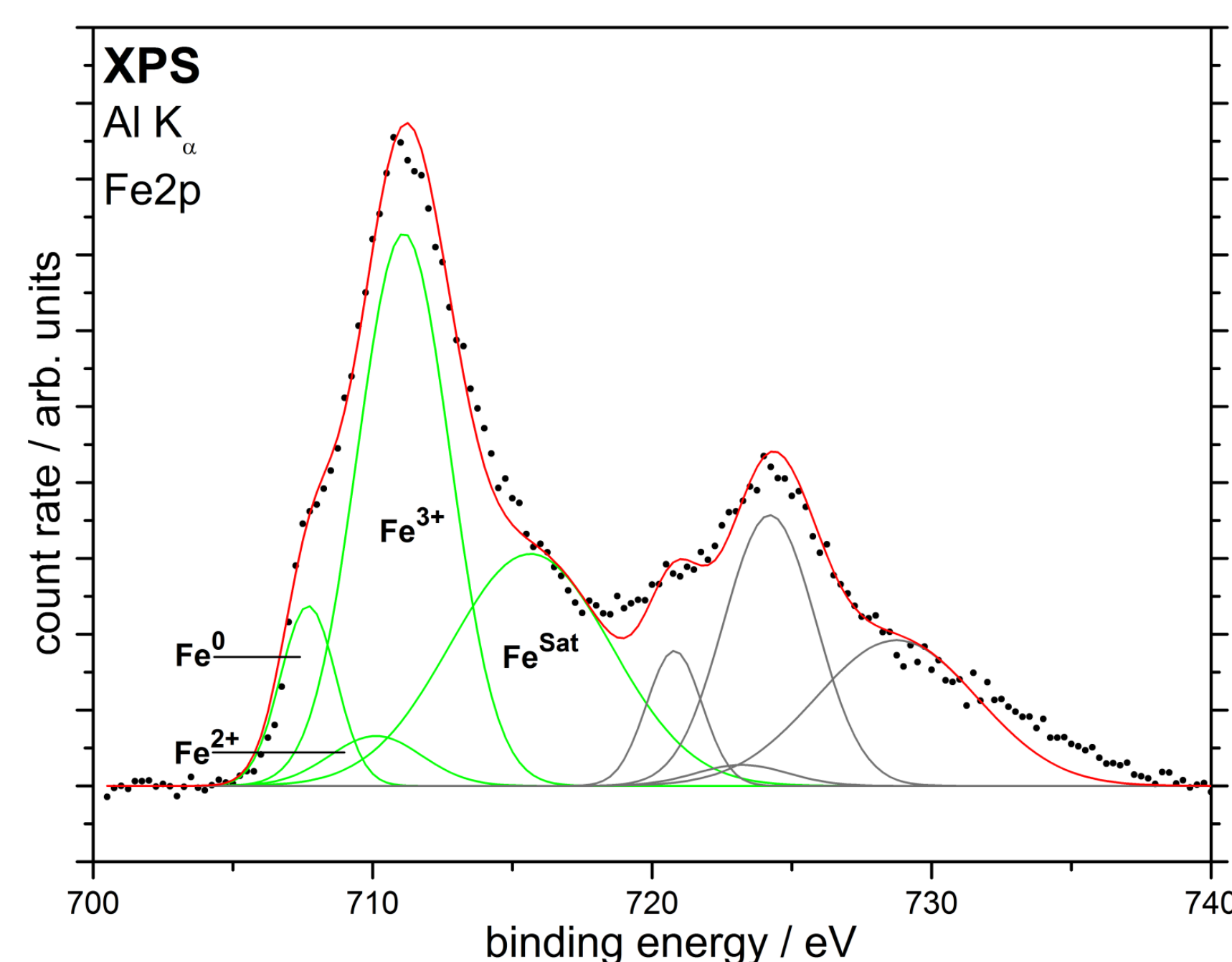
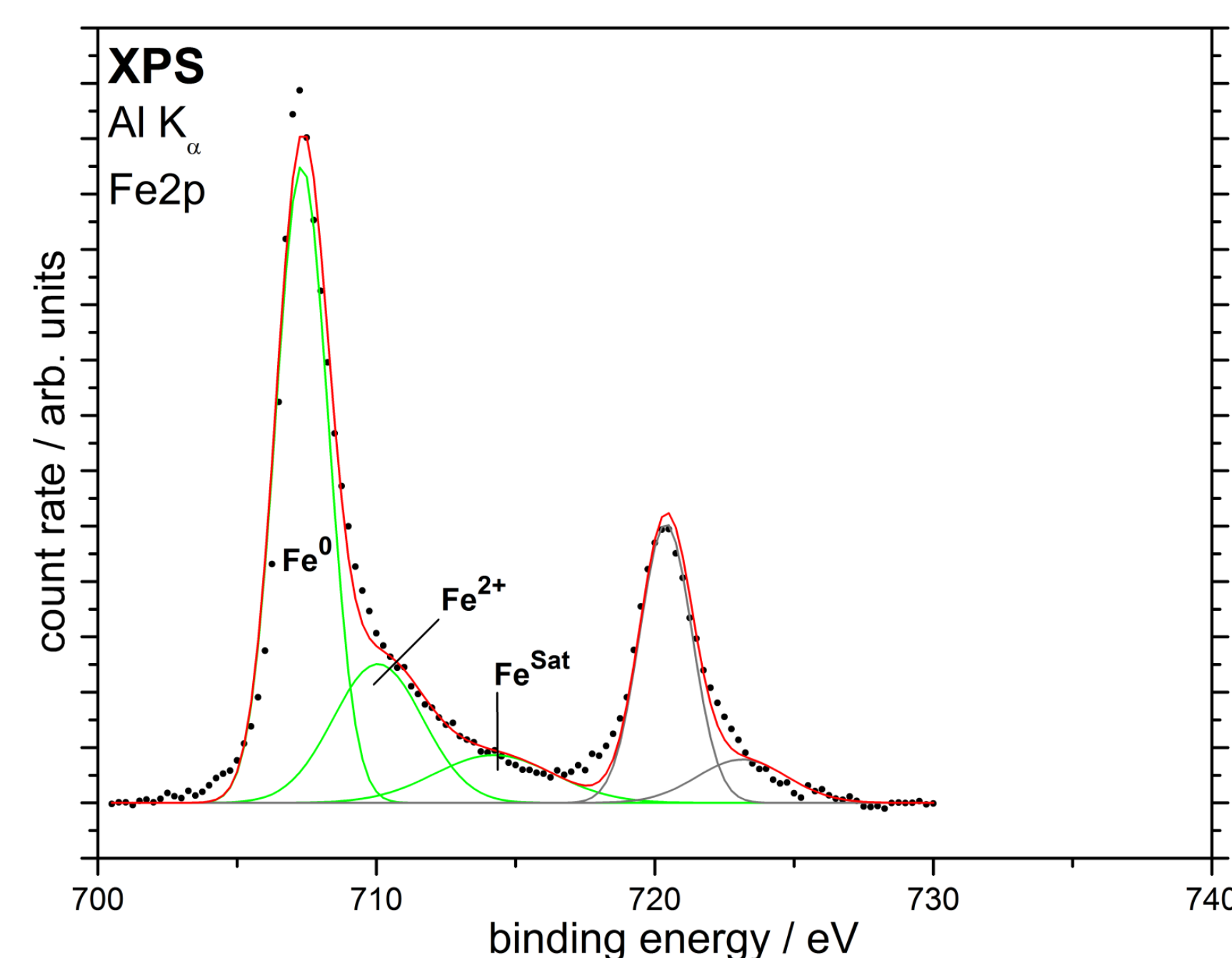


| Orbital | Peak | rel. int. | Assignment |
|---------|----------------|-----------|------------------|
| C1s | C ₀ | 7.6 % | carbide |
| | C ₁ | 50.4 % | C-C / C-H |
| | C ₂ | 22.4 % | C-O |
| | C ₄ | 19.6 % | C=O |
| Fe2p | I | 15.3 % | Fe ⁰ |
| | II | 7.0 % | Fe ²⁺ |
| | III | 77.7 % | Fe ³⁺ |

XPS 3rd step



| Orbital | Peak | rel. int. | Assignment |
|---------|-------------------------------------|-----------|------------------|
| C1s | C ₀ * | - | - |
| | C ₁ * | 54.2 % | C-C / C-H |
| | C ₂ * & C ₃ * | 38.0 % | C-O & epoxy |
| | C ₄ * | 7.8 % | C=O |
| Fe2p | I | 13.3 % | Fe ⁰ |
| | II | 40.4 % | Fe ²⁺ |
| | III | 46.3 % | Fe ³⁺ |



Conclusion

The present study explores insights into the adhesion mechanisms between stainless steel (316L) and industrial, polymeric epoxy adhesives. It is shown how surfaces change topographically as well as in their chemical composition, if epoxy and steel layers get into contact with each other:

Even very carefully and under ultrahigh vacuum conditions cleaned steel surfaces still exhibit significant traces of carbon and oxygen. The interaction between the two materials results in various functional carbon groups like C-C, C-O and C=O and in the reduction of iron at the steel surface from Fe³⁺ to Fe²⁺ according to the different preparation steps. This reduction occurs probably due to the interaction between the functional groups of the epoxy resin and iron oxides. Spin-coating the epoxy resin forms a layer on the steel surface including smooth regions as well as areas covered by clustered epoxy.

Literature

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